

Effect of F Content on the Protection of Melted Magnesium Alloy

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Abstract: The protection of molten AZ91D alloy in the cover gases containing sulfur decomposed by FeS_2 and fluorine produced by HFC-134a at 730 °C was investigated in this paper. The surface films were analyzed by scanning electron microscopy (SEM), energy dispersive spectrometer (EDS), X-ray diffraction (XRD) and X-ray photoelectron spectrometer (XPS). It is revealed that the cover gases containing sulfur decomposed by FeS_2 and fluorine produced by HFC-134a can protect the molten AZ91D alloy well. HFC-134a whose volume fraction is 0.04% -0.1% mixed with gas containing sulfur by adding FeS_2 0.5g per 30 minutes and holding the melting temperature at 730 °C for 30 min can protect the molten AZ91D alloy. The bigger the volume fraction of HFC-134a, the better the effect. The protected film is formed of MgO , MgF_2 and small amount MgS .

Keywords: Magnesium alloy, SEM, FeS_2 , HFC-134a, Oxidation.

1. Introduction

As a structural material, magnesium alloys are more and more widely used in aerospace, automotive, electronics, the field of national defense and bio-medical applications due to their good properties, rich reserves and production cost decreased with the progress of technology. However, molten magnesium oxidizes readily in an atmosphere containing oxygen, often leading to combustion on the melt surface [1]. To address this issue, it is necessary to protect the melt by the cover gas over the melts. SF_6 contained in common gases is no longer acceptable environmentally due to its extremely high greenhouse effect as well as a very long retention period in the atmosphere and substituted by the other atmosphere of gases containing sulfur and fluorine.

Many researchers have reported that 1,1,1,2-tetrafluoroethane (HFC-134a) is a possible substitute for SF_6 and HFC-134a can provide effective protection for magnesium and some magnesium alloy melts [2,3]. Moreover, the protection effects of SO_2 mixed with carrier gases also have been studied by a few researchers which found that MgSO_4 also formed in the protective film and the formation of the film might be related to the formation of MgSO_4 [4-8]. FeS_2 , a kind of pyrites, is decomposed at a high temperature and elemental sulfur created as well as sulfur dioxide [9,10] and has a lower cost compared with SO_2 .

In this paper, the protection of molten magnesium alloys AZ91D in the cover gases containing sulfur decomposed by FeS_2 and fluorine produced by HFC-134a was investigated. With the different contents of sulfur and fluorine, the micro-structure and composition of the surface films were examined, and the thermodynamic properties of the system were also investigated.

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2. Materials and methods

The chemical composition of the material AZ91D magnesium alloy studied at present in weight percent was 9.21%Al, 0.67%Zn, 0.203%Mn, 0.0007%Ni, 0.002%Fe, 0.0006%Cu, and Mg balance.

In order to reduce the influence of surface films, the surface oxide film of magnesium alloy block (130g -170g) was cut and removed before the experiment. The chemical composition of FeS₂ in this experiment was analyzed by EDS and determined as 4.24%O, 0.86%Mg, 2.79%Si, 47.71%S, 44.4%Fe in weight percent. The protective effect using different sizes FeS₂ were compared and determine to use FeS₂ with 120~180 μ m in this experiment.

Figure 1 shows the installation and the schematic diagram of open furnace of 5L used in this experiment. To control the melting atmosphere, a certain count of FeS₂ was put around the crucible with magnesium alloy specimen at the bottom of the open furnace from the filling tube for every 30 min. At the same time, the other controlled mixed gases containing HFC-134a flew through a flow meter and fed into the furnace. The cover gases containing different HFC-134a or air contents were shown in Table 1.

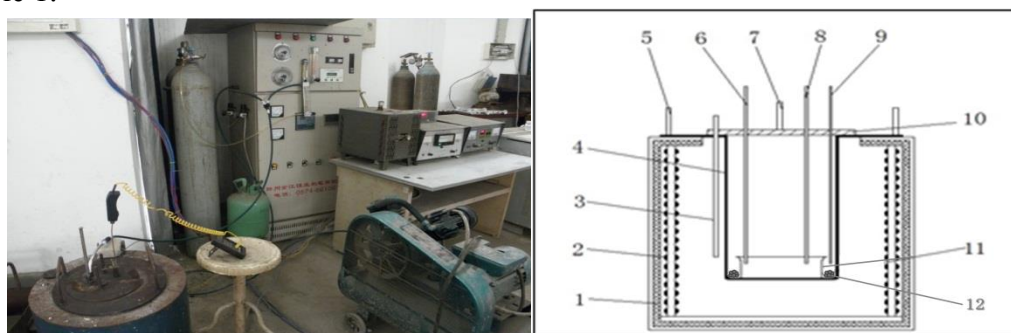


Figure 1. a. Photograph of the installation used in this experiment b. Schematic diagram of apparatus sectional view of the furnace. 1.Heat-barrier materials 2.Resistance wire 3.Thermocouple of temperature control 4.Melting furnace 5.Handle of melting furnace 6.Thermocouple of temperature measurement 7.Handle of furnace cover 8.Inlet pipe 9.Filling tube 10.Furnace cover 11.Crucible.

12. FeS₂. The cover gases pumped in the furnace to replace the air before the experiment for 30 min. Proper amount of FeS₂ was added around the crucible with magnesium alloy specimen at the bottom of the furnace. Then began to heat to 730°C with the speed of 25°C/min. The FeS₂ was added from filling sleeve tube according to set time and amount until the end of the experiment .Cut the volume of 10mm×10mm×8mm out of the specimen to analyze and test. Phase analysis of the protective film was by XRD and morphology and composition by EXEM and accessory of EDS.

3. Results and discussions

3.1. The Effect of HFC-134a Content on Protective Effect

Figure 2 shows the effect of HFC-134a content on protective effect of molten AZ91D alloy with adding FeS₂ 0.5g per 30 min and holding the melting temperature at 730°C for 30 minutes. When volume fraction of HFC-134a was 0%, melting magnesium was protected only by proper amount FeS₂ and some cauliflower-like oxides formed on the surface (Figure 2a). The effect was not good. With volume fraction of HFC-134a 0.04%, a little of the oxides were formed at individual position and effect is common (Figure 2b). With volume fraction of HFC-134a 0.07%, cracking was formed on the film substituting oxides and effect is common (Figure 2c). With volume fraction of HFC-134a 0.1%, a silver-gray dense crack-free protective film with no crack was formed on the surface and the effect is good (Figure 2d). In a word, protective effect is better with higher volume fraction of HFC-134a under the condition that FeS₂ was added 0.5g per 30 min.

Table 1. The parameters and the protection effect of samples

Samples	Weight of $\text{FeS}_2(\text{g})$ per 30min	Volume fraction of HFC-134a/%	Protection effect
1	0.5	0	Not protected
2	0.5	0.04	Partly protected
3	0.5	0.07	Partly protected
4	0.5	0.1	Fully protected



a. 0% HFC-134a+0.5g FeS_2



b. 0.04% HFC-134a+0.5g FeS_2

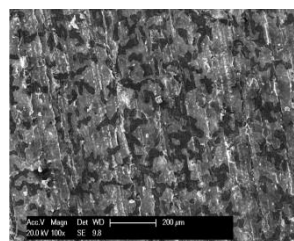


c. 0.07% HFC-134a+0.5g FeS_2

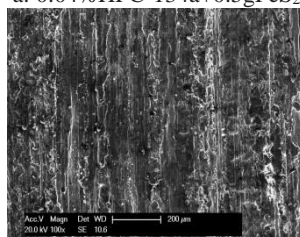
Figure 2. The effect of HFC-134a content on protective effect (0.5g FeS_2 /30min-air-730°C-holding 30min)

3.2. Morphology of Surface Film

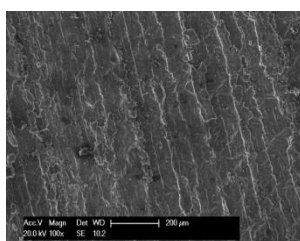
Figure 3 shows the different surface film morphology of molten AZ91D alloy protected by different HFC-134a content with adding FeS_2 0.5g per 30 min and holding the melting temperature at 730°C for 30 min. With volume fraction of HFC-134a 0.04%, a part of the matrix was exposed and the surface film was not complete (Figure 3a). With volume fraction of HFC-134a 0.07%, most of the matrix was covered by protected film with a little cracking and the surface film was become compact (Figure 3b). With volume fraction of HFC-134a 0.1%, compact protective film with no crack was formed and covered the matrix completely with a good effect (Figure 3c).



a. 0.04%HFC-134a+0.5gFeS₂



b. 0.07%HFC-134a+0.5gFeS₂



c. 0.1%HFC-134a+0.5gFeS₂

Figure 3. Morphology of the surface film tested by EXEM (0.5g FeS₂/30min-air-730°C-holding 30min)

3.3. Compositions of Surface Film

Table 2 shows the effect of HFC-134a content on composition of surface film with adding FeS₂ 0.5g per 30 min and holding the melting temperature at 730°C for 30 min. Surface film was tested by EDS and average composition can be determined. The depth tested by EDS can be greater than the thickness of surface film which was thin. Although magnesium matrix information was tested, reaction degree can be judged. With volume fraction of HFC-134a/% increasing, the percentage content of F increased, O decreased obviously and S decreased also. The content of MgO and MgS decreased and MgF₂ increased in the film judged by the percentage content of O, F and S.

Table 2. Different compositions of surface film with the change of HFC-134a content
Sample parameters: AZ91D alloy, 0.5g FeS₂/30min-air-730°C- 30min

Volume fraction of HFC-134a/%	O/%	F/%	S/%	Mg/%
0.04%	26.05	10.55	3.14	53.26
0.07%	20.15	15.06	2.63	58.22
0.1%	18.93	18.34	1.38	52.88

3.4. Analysis of XRD and XPS

The protected film contains not only Mg, F, O and S, but also other elements determined by the testing of morphology and compositions. Compounds can be determined by XRD analysis. Figure 4 shows the XRD analysis result of the AZ91D alloy sample. The melt magnesium alloy was protected by mixed gas containing 0.1% HFC-134a and sulfur decomposed by FeS₂ which was added 0.5g per 30 minutes. Heat the melting to the temperature at 730°C and hold for 30 minutes. It can be concluded that the protected film was formed of MgO, MgF₂ and a small amount of MgS. The peak of Mg is obvious and caused by matrix with thin surface film (Figure 4).

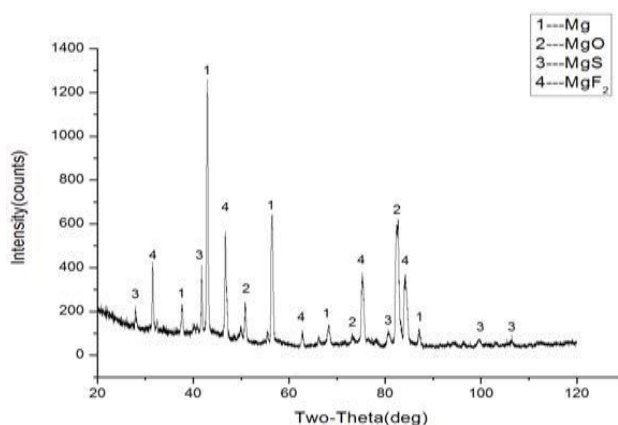


Figure 4. XRD analysis of the protected film

Figure 5 shows the whole pattern of surface film and the film sputtered for 500s by XPS. The sample melted in the protective gas containing 0.1% HFC-134a and sulfur decomposed by FeS₂ which was added 0.5g per 30 minutes. The surface film contains Mg, O, F, S and a little C. Figure 6 shows the Mg1sXPS spectra of film from the same sample. 3 peaks can be obtained by fitting the high resolution spectra. It means Mg elements existed in 3 states in the protected film. It can be concluded that the main elements Mg, O, S and F in the film correspond to peaks of MgO, MgS and MgF₂.

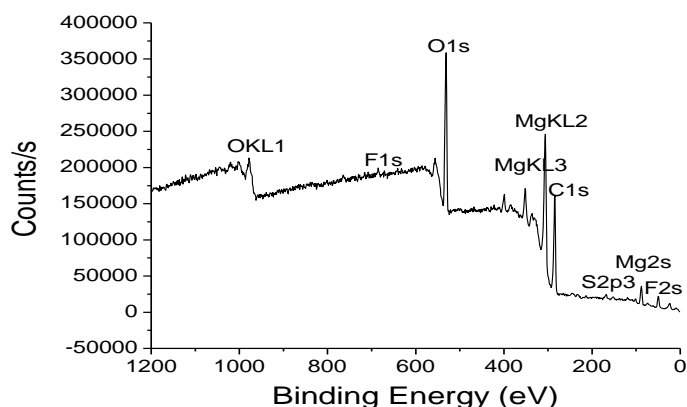


Figure 5. The whole pattern of surface film determined by XPS (730°C-30min-air-0.5g FeS₂/30min+0.1% HFC-134a)

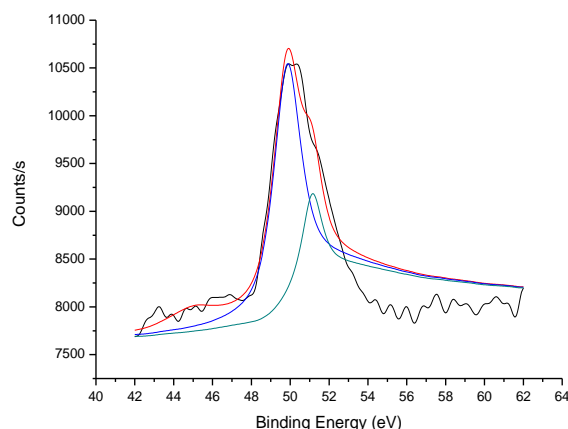


Figure 6. Mg1sXPS spectra of the surface film
(730°C-30min-air-0.5gFeS₂/30min+0.1%HFC-134a)

4. Conclusions

Finally, the basic questions posed above are then discussed and conclusions are drawn.

(1) The cover gases containing sulfur decomposed by FeS₂ and fluorine produced by HFC-134a can protect the molten AZ91D alloy well.

(2) Volume fraction of HFC-134a was 0.04% -0.1% mixed with gas containing sulfur by adding FeS₂ 0.5g per 30 min and holding the melting temperature at 730°C for 30 min can protect the molten AZ91D alloy. The bigger the volume fraction of HFC-134a, the better the effect.

(3) The protected film was formed of MgO, MgF₂ and small amount MgS.

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References

1. MIRAK, A., DAVIDSON, C. J., TAYLOR, J. A., Characterisation of fresh surface oxidation films formed on pure molten magnesium in different atmospheres. *Corr. Sci.*, **52**, 2010,1992–2000.
2. RICKETTS, N. J., CASHION, S. P., Hydrofluorocarbons as cover gases for magnesium melt protection, Magnesium Technology 2006[C]. Warrendale, USA. *Min. Met. Mater. Soc.*, 2001, 31-36.
3. CASHION, S. P., RICKETTS, N. J., FROST, M. T., KORN, C. J., The protection of molten magnesium and its alloys during die-casting[C], The 8th Annual IMA Magnesium in Automotive Seminar. Aalen, GER. *Int. Magnes. Assoc.*, 2000, 12-14.
4. FRUEHLING, J. F., Protective Atmospheres for Molten Magnesium [D]. Ph.D.Thesis. *Univ. Michigan.*, 1970.
5. ARGO, D., LEFEBVRE, M., Magnesium Technology 2003 [M], TMS. San Diego, America., 2003, 15-21.
6. CASHION, S. P., The Use of Sulphur Hexa-uoride (SF₆) for Protecting Molten Magnesium[D]. Ph.D. Thesis. *Univ. Queensland.*, 1998.
7. PETTERSEN, G., VRELID, E., TRANELL, G., [M]. *Eng.A. Mater. Sci.*, **332**, 2002, 285-294.
8. WANG, X. F., XIONG, S. M., *Mater. Chem. Phys.*, **135**, 2012, 541-548.
9. ZENGHUI, W., HELIN, L., XIAOPENG, X., Study and Characteri-zation of Reduced Sulfur in Oxidation Process of Ferro Sulfide Compounds. *Min. Metalurg.*, **18**(1), 2009, 96-99.



10. FEI, X., YONGMING, H., CHANGDONG, S., Decomposition Char-acteristics of Pyrite (FeS_2) Particle under Combustion Condition. *J. Combust. Sci. Technol.*, **6**(3), 2000, 280-283.
11. Xu, Z., Chen, X., Meng, L., Yu, M., Li, L., Shi, W., Sample Consensus Model and Unsupervised Variable Consensus Model for Improving the Accuracy of a Calibration Model. *Appl. Spect.*, **73**(7), 2019, 747-758.
12. LEI, Z., GAO, H., CHANG, X., ZHANG, L., WEN, X., & WANG, Y., An application of green surfactant synergistically metal supported cordierite catalyst in denitration of Selective Catalytic Oxidation. *J. Clean. Prod.*, **249**, 2020, 119307.
13. ZHANG, Y., ZHANG, X., LI, M., LIU, Z., Research on heat transfer enhancement and flow characteristic of heat exchange surface in cosine style runner. *Heat and Mass Transfer*, **55**(11), 2019, 3117-3131.
14. LUPESCU, S., ISTRATE, B., MUNTEANU, C., MINCIUNA, M.G., FOCSANEANU, S., EARAR, K., Characterization of Some Master Mg-X System (Ca, Mn, Zr, Y) Alloys Used in Medical Applications. *Rev.Chim.*, **68**(6), 1310-1315.

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